

# Well Test Interpretation

## SKM4323

# CONVENTIONAL INTERPRETATION METHODS

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# WEEK 05



# After Varying Flow Rates

- A test after varying flow rates is interpreted using the flow rate superposition principle discussed before:

$$p_i - p_{wf}(t) = \frac{B\mu}{2\pi kh} \sum_{i=1}^n (q_i - q_{i-1}) p_D(t - t_{i-1}) \quad (4.30)$$

- Once the wellbore storage affect has ended, the pressure variations are given by equation (4.3). Equation (4.30) becomes

$$p_i - p_{wf}(t) = \frac{B\mu}{4\pi kh} \sum_{i=1}^n (q_i - q_{i-1}) \left( \ln \frac{K(t - t_{i-1})}{r_w^2} + 0.81 + 2S \right) \quad (4.31)$$



## After Varying Flow Rates.../2

- The interpreter is interested in the pressure variations since the last change in flow rate,  $t_{n-1}$ . The pressure variation at the time when the change took place is:

$$p_i - p_{wf}(t_{n-1}) = \frac{B\mu}{4\pi kh} \sum_{i=1}^{n-1} (q_i - q_{i-1}) \left( \ln \frac{K(t_{n-1} - t_i)}{r_w^2} + 0.81 + 2S \right)$$

# After Varying Flow Rates.../3

- The pressure buildup since the time when the well was shut in is expressed by

$$p_{ws}(\Delta t) - p_{wf}(t_{n-1}) = \frac{B\mu}{4\pi kh} \left\{ \sum_{i=1}^{n-1} (q_i - q_{i-1}) \ln \frac{t_{n-1} - t_{i-1}}{t_{n-1} - t_{i-1} + \Delta t} - (q_n - q_{n-1}) \left( \ln \frac{K \Delta t}{r_w^2} + 0.81 + 2S \right) \right\}$$

**(4.32)**

$\Delta t$  is the time elapsed since the last change in flow rate.



# After Varying Flow Rates.../4

- It can be written as follows:

$$p_{ws}(\Delta t) - p_{wf}(t_{n-1}) = \frac{162.6 B\mu}{kh} \left\{ \sum_{i=1}^{n-1} (q_i - q_{i-1}) \log \frac{t_{n-1} - t_{i-1}}{t_{n-1} - t_{i-1} + \Delta t} - (q_n - q_{n-1}) \left( \log \Delta t + \log \frac{k}{\phi \mu c_t r_w^2} - 3.23 + 0.87 S \right) \right\}$$

(in practical US units) **(4.33)**

$$p_{ws}(\Delta t) - p_{wf}(t_{n-1}) = \frac{21.5 B\mu}{kh} \left\{ \sum_{i=1}^{n-1} (q_i - q_{i-1}) \log \frac{t_{n-1} - t_{i-1}}{t_{n-1} - t_{i-1} + \Delta t} - (q_n - q_{n-1}) \left( \log \Delta t + \log \frac{k}{\phi \mu c_t r_w^2} - 3.10 + 0.87 S \right) \right\}$$

(in practical metric units) **(4.34)**



# After Varying Flow Rates.../5

## Interpretation

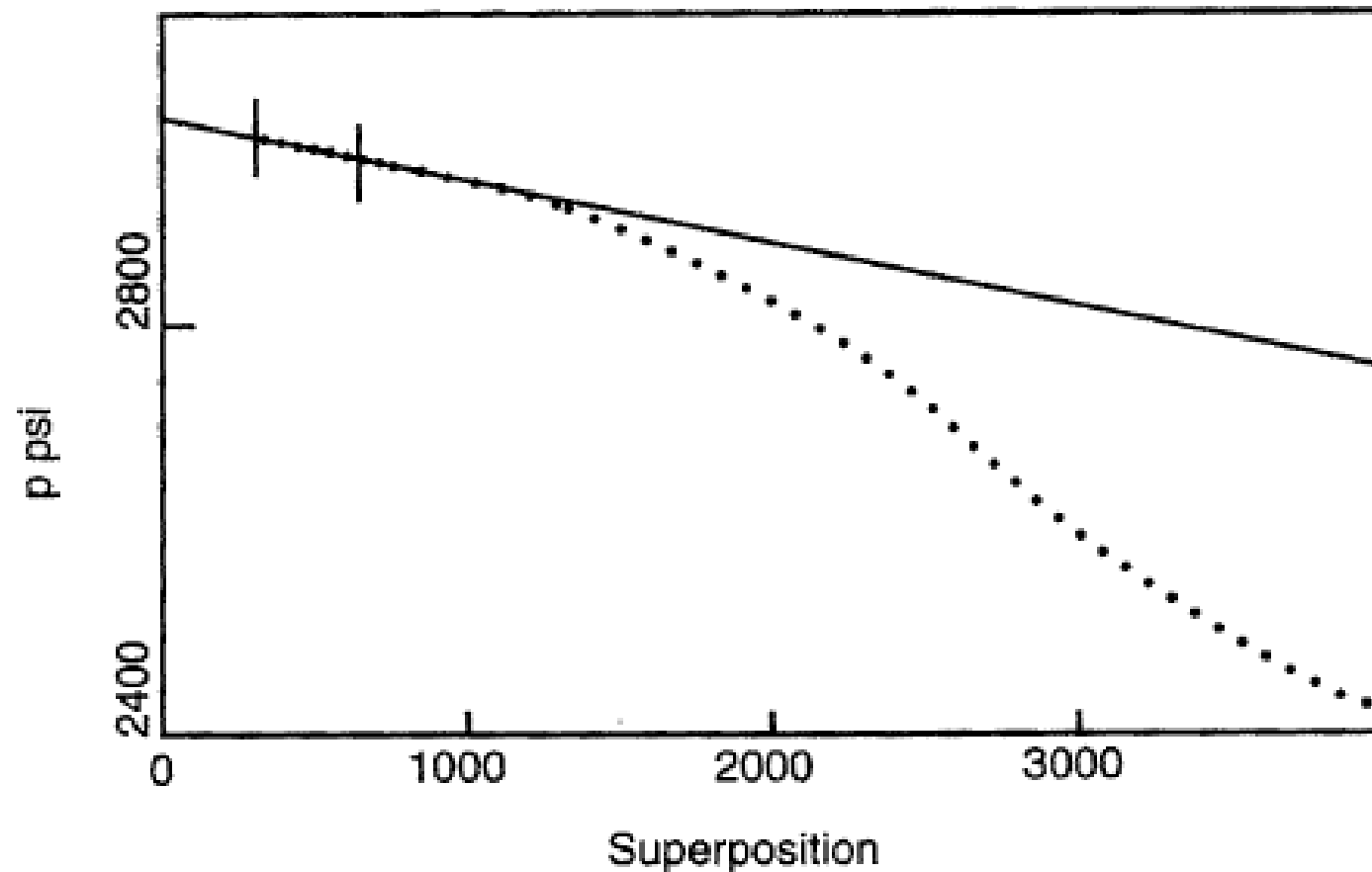
- The pressure varies linearly versus the right-hand member (between parentheses) of equations (4.33) and (4.34). The member is a function of flow rates and time and is called the superposition function.
- If the value of pressure measured in the bottom of the hole is plotted versus the superposition function, a straight line a slope of  $m$  can be seen once the effect of wellbore storage has ended.

$$m = \frac{162.6 B\mu}{kh} \quad (\text{in practical US units}) \quad (4.35)$$

$$m = \frac{21.5 B\mu}{kh} \quad (\text{in practical metric units}) \quad (4.36)$$



# After Varying Flow Rates.../6



**Fig. 4.7**



# After Varying Flow Rates.../7

## Interpretation

- The slope is independent of flow rate. This is the advantage of the representation: the results obtained with different flow rates can be compared on the same graph.
- To find an expression of  $m$  which is dependent on flow rate comparable to what is obtained with Horner's method, the superposition function needs only to be divided by the last flow rate.

# After Varying Flow Rates.../8

## Interpretation

- The slope,  $m$ , of the straight line is used to determine the reservoir's **kh**:

$$kh = \frac{162.6 B\mu}{m} \quad (\text{in practical US units}) \quad (4.37)$$

$$kh = \frac{21.5 B\mu}{m} \quad (\text{in practical metric units}) \quad (4.38)$$



# After Varying Flow Rates.../9

## Interpretation

- The skin is determined based on the pressure value read on the straight line 1 hour after a last flow rate variation:

$$S = 1.151 \left( \frac{p_{1h} - p_{wf}(t_{n-1})}{(q_{n-1} - q_n) m} - \log \frac{k}{\phi \mu c_t r_w^2} + 3.23 \right) \quad (\text{US}) \quad (4.39)$$

$$S = 1.151 \left( \frac{p_{1h} - p_{wf}(t_{n-1})}{(q_{n-1} - q_n) m} - \log \frac{k}{\phi \mu c_t r_w^2} + 3.10 \right) \quad (\text{metric}) \quad (4.40)$$



# After Varying Flow Rates.../10

## Interpretation

- If the last flow rate variation is a shut-in, the pressure reading for infinite time, i.e. for value of the superposition function equal to zero, is used to determine the extrapolated reservoir pressure.



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# Example 4

(In-class workshop)





# Simplification of the Flow Rate History

- To analyze the final buildup, the simplest method consists in reducing the flow rate history to one single rate and using Horner's method for the actual interpreting.
- The single-rate production data that replace the n-1 multirate reality must be governed by the following principle:
  - flow rate = the last rate;
  - equivalent production time:

$$t_{pe} = \frac{\sum_{i=1}^{n-1} q_i (t_i - t_{i-1})}{q_n} \quad (4.41)$$



## Simplification of the Flow Rate History.../2

- The production time is designed to provide a total production value identical to the production that was actually recorded.
- The real production time should not be used to compute and equivalent flow rate.

# Buildup Radius of Investigation

- The theoretical radius of investigation depends only on the **duration of the pressure buildup**.
- The radius of investigation can be estimated by using the formula proposed before:

$$r_i = 0.032 \sqrt{\frac{kt}{\phi \mu c_t}} \quad (\text{in practical US units}) \quad (4.42)$$

$$r_i = 0.038 \sqrt{\frac{kt}{\phi \mu c_t}} \quad (\text{in practical metric units}) \quad (4.43)$$





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# Example 5

(In-class workshop)



# References

1. Bourdarot, Gilles : Well Testing: Interpretation Methods, Éditions Technip, 1998.
2. Internet.

