

CHEMICAL REACTION ENGINEERING (SKF3223)

Chapter 1: Mole Balances

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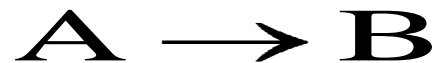


Rate of Reaction

- The reaction rate is the rate at which a species loses its chemical identity per unit volume.
- **RATE = SPEED**
- The **RATE** of a reaction is the **SPEED** at which a reaction happens.
- If a reaction has a **low rate** that means the molecules combine at a **slower speed** than a reaction with a high rate.

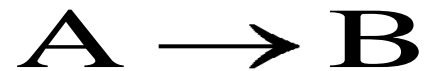
Rate of Reaction

- The rate of a reaction can be expressed as **the rate of disappearance of a reactant** or as the **rate of appearance of a product**.
- Consider species A:



- r_A = the rate of formation of species A per unit volume
 - $-r_A$ = the rate of a disappearance of species A per unit volume
 - r_B = the rate of formation of species B per unit volume
- r_A tells us how fast a number of moles of one chemical species are being consumed to form another chemical species.

Example:



If B is being created at 0.6 moles per decimeter cubed per second, therefore:

The rate of formation of B is : $r_B = 0.6 \text{ mole/dm}^3/\text{s}$

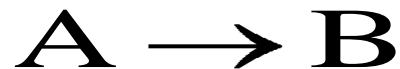
The rate of a disappearance of species A is :

$$-r_A = 0.6 \text{ mole/dm}^3/\text{s}$$

The rate of formation of A is : $r_A = -0.6 \text{ mole/dm}^3/\text{s}$

Remember.... r_B

- r_B is the rate of formation of species B per unit volume [e.g. mol/dm³s]
- r_B is a function of concentration, temperature, pressure, and the type of catalyst (if any)
- r_B is independent of the type of reaction system (batch, plug flow, etc.)
- r_B is an algebraic equation, **not** a differential equation



Reaction rate

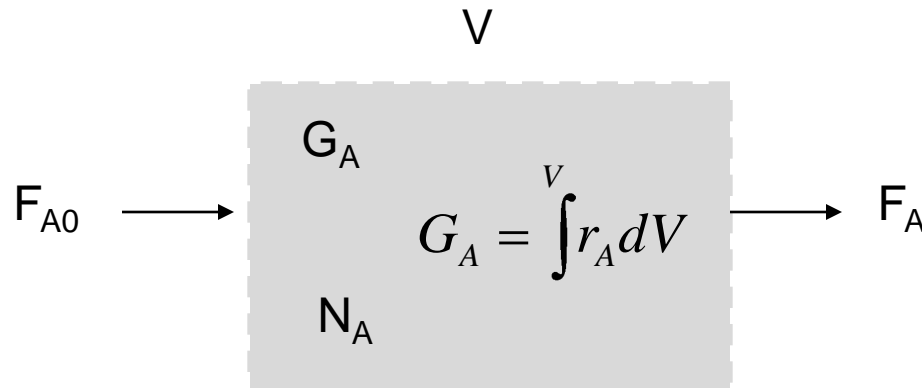
- Reaction rate, r is a function of concentration, for example:

$$-r_A = kC_A \text{ (First order reaction)}$$

$$-r_A = kC_A^2 \text{ (Second order reaction)}$$

$$k = \text{specific reaction rate (time}^{-1}\text{)}$$

General Mole Balance Equation (GMBE)



F_{A0} = Entering molar flow rate of A (mol/time)

F_A = Exiting molar flow rate of A (mol/time)

G_A = Rate of generation(formation) of A (mol/time)

V = Volume (m^3)

r_A = rate of generation(formation) of A (mole/time.vol)

N_A = number of moles of A inside the system Volume V (mols)

General Mole Balance Equation

$$[\text{In}] + [\text{Generation}] - [\text{Out}] = [\text{Accumulation}]$$

$$F_{in} + G - F_{out} = \frac{dN}{dt}$$

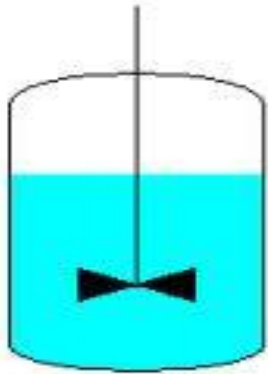
moles/time moles/time moles/time moles/time

$$F_{in} + \int r \cdot dV - F_{out} = \frac{dN}{dt}$$

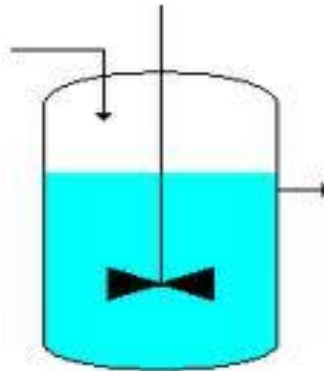
moles/time $\frac{\text{moles}}{\text{time} \cdot \text{volume}} \cdot \text{volume}$ moles/time moles/time

- Develop the design equation for the various types of industrial reactors (batch, semibatch, and continuous-flow)

Types of Reactors

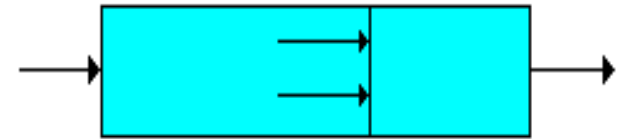


Batch

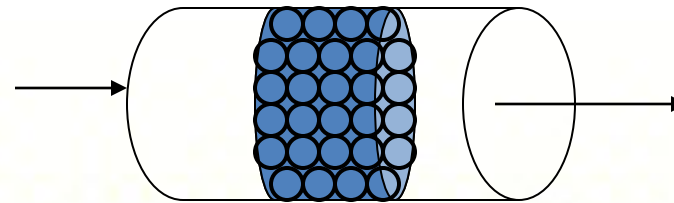


CSTR

Continuos Flow



Tubular/Plug Flow



Packed Bed

BATCH REACTOR



No inflow or outflow

$$r = \frac{dN}{dt} \cdot \frac{1}{V}$$

Assumption

- $F_{in} = F_{out} = 0$
- V is constant (well-mixed)

- Small scale operation
- For testing new processes
- To manufacture expensive product
- ADV: high conversion
- DISADV: high labor cost
- Not reproducible

Batch reactor derivation

Well-mixed

$$\int r_A dV = r_A V$$

$$\frac{dN_A}{dt} = r_A V$$

Differential form

Rearranging and integrating with limits

$$\begin{array}{l} t = 0 \quad N_A = N_{A0} \\ t = t_1 \quad N_A = N_{A1} \end{array}$$

$$t_1 = \int_{N_{A0}}^{N_{A1}} \frac{dN_A}{r_A V}$$

The time necessary to reduce the number of moles from N_{A0} to N_{A1} and also to from N_{B1} mole of B -- graph of reaction (N_A , t)

Multiplying by -1 and changing the limits of integration

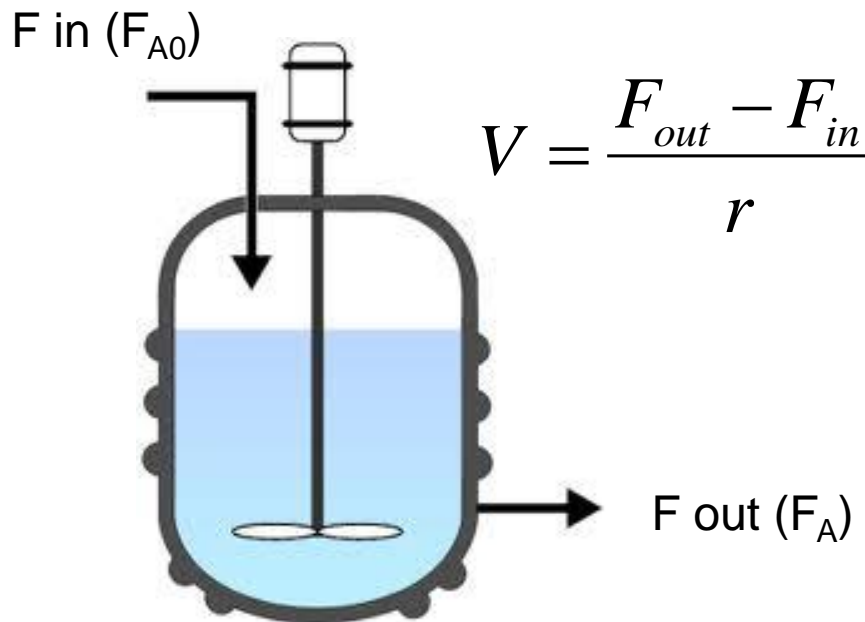
$$t_1 = \int_{N_{A1}}^{N_{A0}} \frac{dN_A}{-r_A V}$$

Integral form

CONTINUOUS-STIRRED TANK REACTOR (CSTR)

Assumption

- Well mixed – constant concentration, temperature, reaction rate
- No accumulation



- Commonly used in industry
- Liquid-phase reaction
- Advantage: when intense agitation is required
- Disadvantage: larger reactor are necessary to obtain high conversion

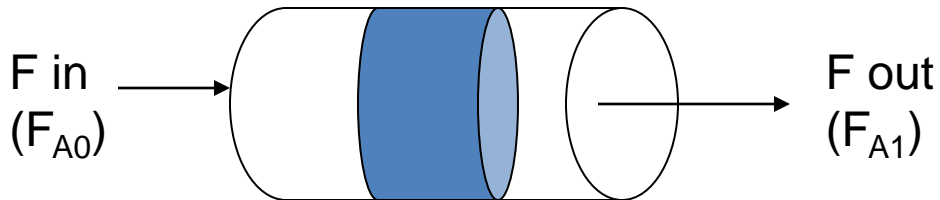
The volume of the reactor

$$V = \frac{F_{A0} - F_A}{-r_A}$$

Algebraic form

TUBULAR REACTOR OR PLUG-FLOW REACTOR (PFR)

Assumption: Operated at steady state



- ❑ Consists of a cylindrical pipe
- ❑ Gas-phase reaction
- ❑ Advantages: easy to maintain, provides the highest conversion
- ❑ Disadvantage: difficult to maintain the temperature within the reactor

$$r = \frac{F_{out} - F_{in}}{dV}$$

$$r_A = \frac{dF_A}{dV}$$

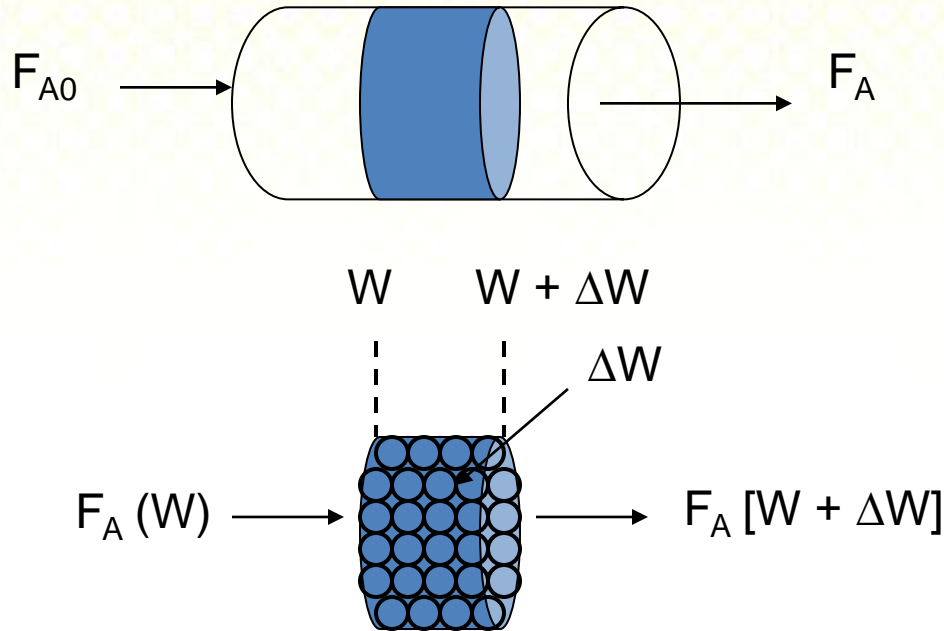
Differential form

The volume necessary to reduce the entering molar flow rate of A from F_{A0} to F_{A1} or the volume necessary to produce a molar flow rate of B of F_{B1} – graph of reaction (F_{A0} , V)

$$V_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r_A}$$

Integral form

PACKED-BED REACTOR (PBR)



- The reaction rate is based on mass of solid catalyst, W
- Fluid-solid heterogeneous reaction
- Essentially tubular reactor that is packed with solid catalyst particles

Differential form

$$\frac{dF_A}{dW} = r'_A$$

Integral form

$$W_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r'_A}$$

Catalyst weight necessary to reduce the entering molar flow rate of A, F_{A0} to F_{A1}
 – graph of reaction (F_A , W)

Differential form

Algebraic form

Integral form

BATCH

$$\frac{dN_A}{dt} = r_A V$$

$$V = \frac{F_{A0} - F_A}{-r_A}$$

$$t_1 = \int_{N_{A1}}^{N_{A0}} \frac{dN_A}{-r_A V}$$

CSTR

$$r_A = \frac{dF_A}{dV}$$

$$V_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r_A}$$

PFR

$$\frac{dF_A}{dW} = r'_A$$

$$W_1 = \int_{F_{A1}}^{F_{A0}} \frac{dF_A}{-r'_A}$$

PBR

REFERENCES

Main Reference:

1. Fogler, H.S., "*Elements of Chemical Reaction Engineering*", 4th Edition, Prentice Hall, New Jersey, 2006.

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1. Davis, M.E and Davis, R.J, "*Fundamentals of Chemical Reaction Engineering*", Mc-Graw-Hill, New York, 2003
2. Schmidt, L.D, "*The Engineering of Chemical Reactions*", Oxford, New York, 1998
3. Levenspiel, O., "*Chemical Reaction Engineering*", 3rd Edition, Wiley, New York, 1998
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