

SKF 3143

Process Control and Dynamics: Response of Second Order Systems

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Learning Objectives

When I complete this chapter, I want to be able to do the following:

1. Analyze the response of the second order systems





Here

- A second-order transfer function can arise physically whenever two first-order processes are connected in series.
- For example, two stirred-tank heaters, each with first-order transfer function relating inlet to outlet temperature, might be physically connected so the outflow stream of the first heater is used as the inflow stream of the second tank.

• In this chapter we consider the case where the second-order transfer function has the standard form

$$G_{(s)} = \frac{K}{\tau^2 s^2 + 2\zeta \tau s + 1}$$
(7.2)

Where ζ (zeta)= damping coefficient (dimensionless)





 The type of behavior that occur depends on the numerical value of damping coefficient, ζ:

It is convenient to consider three types of behavior:

Damping Coefficient	Types of Response	<i>Root of Characteristic Polynomial</i>
ζ > 1	Overdamped	Real and unequal
ζ = 1	Critically damped	Real and equal
0 < ζ < 1	Underdamped	Complex conjugates

- What about $\zeta < 0$? It results in unstable system
- The characteristic polynomial is the denominator of the transfer function:

$$\tau^2 s^2 + 2\zeta \tau s + 1$$





- The transfer function given by Eqs. 7.1 and 7.2 differ only in the denominators.
- Equating them yields the relation between the two alternative forms for the *overdamped* second-order case.
- Note that when $\zeta \ge 1$, the denominator of 7.2 can be factored as:

$$\tau^2 s^2 + 2\zeta \tau s + 1 = (\tau_1 s + 1)(\tau_2 s + 1)$$
(7.3)

 Expanding the right side of 7.3 and equating coefficients of the s terms, yields

$$\tau^2 = \tau_1 \tau_2$$
$$2\zeta \tau = \tau_1 + \tau_2$$

from which we obtain

$$\tau = \sqrt{\tau_1 \tau_2}$$
$$\zeta = \frac{\tau_1 + \tau_2}{2\sqrt{\tau_1 \tau_2}}$$





• Alternatively, the left side of 7.3 can be factored:

$$\tau^{2}s^{2} + 2\zeta\tau s + 1 = \left(\frac{\tau s}{\zeta - \sqrt{\zeta^{2} - 1}} + 1\right)\left(\frac{\tau s}{\zeta + \sqrt{\zeta^{2} - 1}} + 1\right)$$
(7.4)

from which expression for τ_1 and τ_2 are obtained

$$\tau_{1} = \frac{\tau}{\zeta - \sqrt{\zeta^{2} - 1}} \qquad (\zeta \ge 1) \qquad (7.5)$$

$$\tau_{2} = \frac{\tau}{\zeta + \sqrt{\zeta^{2} - 1}} \qquad (\zeta \ge 1) \qquad (7.6)$$





Step Response

• For the step input with transform:

$$Y_{(s)} = \frac{KM}{s(\tau^2 s^2 + 2\zeta \tau s + 1)}$$
(7.7)

 After some manipulation, and inverting to the time domain, three forms of response are obtained:

Case a (ζ > 1)

If the denominator of Eq. 7.7 is factored using Eqs. 7.5 and 7.6, then the response can be written

$$y_{(t)} = KM \left(1 - \frac{\tau_1 e^{-t/\tau_1} - \tau_2 e^{-t/\tau_2}}{\tau_1 - \tau_2} \right)$$
(7.8)

If the denominator of Eq. 7.7 is left unfactored, then the response can be written in the equivalent form

$$y_{(t)} = KM \left\{ 1 - e^{-\zeta t/\tau} \left[\cosh\left(\frac{\sqrt{\zeta^2 - 1}}{\tau}t\right) + \frac{\zeta}{\sqrt{1 - \zeta^2}} \sinh\left(\frac{\sqrt{\zeta^2 - 1}}{\tau}t\right) \right] \right\}$$
(7.9)





Case b (
$$\zeta = 1$$
)

$$y_{(t)} = KM \left[1 - \left(1 + \frac{t}{\tau} \right) e^{-t/\tau} \right] \qquad (7.10)$$
Case c ($0 \le \zeta < 1$)

$$y_{(t)} = KM \left\{ 1 - e^{-\zeta t/\tau} \left[\cos \left(\frac{\sqrt{1 - \zeta^2}}{\tau} t \right) + \frac{\zeta}{\sqrt{1 - \zeta^2}} \sin \left(\frac{\sqrt{1 - \zeta^2}}{\tau} t \right) \right] \right\} \qquad (7.11)$$

Several general remarks can be made concerning the responses shown in Figs. 7.1 and 7.2:

- 1. Responses exhibiting oscillation and overshoot (y/KM > 1) are obtained only for values of ζ less than one.
- 2. Large values of ζ yield a sluggish (slow) response.
- The fastest response without overshoot is obtained for the critically damped case ($\zeta = 1$).





Step response of underdamped secondorder systems







Step response of critically-damped and overdamped second-order systems



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- Control system designers often attempt to make the setpoint step response of the controlled variable approximate the step response of underdamped second-order system.
- That is, make it exhibit a prescribed amount of overshoot and oscillation as it settles at the new operating point.
- Values of ζ in the range 0.4 to 0.8 often are suitable for specifying a desired control system response, assuming that it can be approximated as an underdamped second-order system.
- In this range, the controlled variable y reaches the new operating point faster than with $\zeta = 1$ or 1.5, but the response is much less oscillatory (it settles faster) than with $\zeta = 0.2$.





Performance characteristics for the step response of an underdamped process.







- **1. Rise Time.** t_t is the time the process output takes to first reach the new steady-state value.
- **2. Time to First Peak.** t_p is the time required for the output to reach its first maximum value.
- 3. Settling Time. t_s is defined as the time required for the process output to reach and remain inside a band whose width is equal $\pm 5\%$ of the total change in y. The term 95% response time sometimes is used to refer to this case. Also, values of $\pm 1\%$ sometimes are used.
- 4. **Overshoot.** OS = a/b (% overshoot is 100a/b).
- **5. Decay Ratio.** DR = c/a (where *c* is the height of the second peak).
- 6. Period of Oscillation.*P* is the time between two successive peaks or two successive valleys of the response.





References:

- Seborg, D. E., Edgar, T. F., Mellinchamp, D. A. (2003). *Process Dynamics and Control*, 2nd. Edition. John Wiley, ISBN: 978-04-71000-77-8.
- Marlin, T. E. (2000). Process Control: Designing Processes and Control System for Dynamic Performance, 2nd. Edition. McGraw Hill, ISBN: 978-00-70393-62-2.
- Stephanopoulos, G. (1984). *Chemical Process Control. An Introduction to Theory and Practice*. Prentice Hall, ISBN: 978-01-31286-29-0