

SKF 3143

Process Control and Dynamics: Response of First Order Systems

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Learning Objectives

When I complete this chapter, I want to be able to do the following:

1. Analyze the response of the first order systems





Response of First-Order Systems

- The dynamic response of many processes and control system components can be represented by linear first-order differential equations.
- We refer to these processes as *first-order systems*.
- This section presents the response of first-order systems to three different types of input signals: a step function, a ramp, and a sine wave.
- The objective is to learn how the parameters of first-order systems affect their response so that later we can infer the important characteristics of the response of a system by simply examining its transfer function.
- First-order systems are also important because many higher-order systems can be treated as combinations of first-order systems in series and parallel.





Response of First-Order Systems

Consider the linear first-order differential equation:

$$a_1 \frac{dy_{(t)}}{dt} + a_0 y_{(t)} = bx_{(t)} + c \tag{6.1}$$

where y is the output or dependent variable; x is the input variables; t is time, the independent variable; and the parameters a_1 , a_0 , b, and c are constant.

We can write the equation at the initial steady-state.

 $Y_{(t)} =$

$$a_0 y_{(0)} = b x_{(0)} + c \tag{6.2}$$

Note that this equation establishes a relationship between the initial values of x• and y. Subtracting Eq. 6.2 from Eq. 6.1 results in

$$a_{1}\frac{dY_{(t)}}{dt} + a_{0}Y_{(t)} = bX_{(t)}$$
(6.3)
where

$$Y_{(t)} = y_{(t)} - y_{(0)}$$
 are the deviation variables.
 $X_{(t)} = x_{(t)} - x_{(0)}$





Response of First-Order Systems

- Eq. 6.3 is the general linear first-order differential equation in terms of the deviations of the input and output variables from their initial steady-state values.
- In process control it is customary to divide by the coefficient of the output variable, *a*₀.
- Such an operation results in the following equation called the *standard form* of the linear first-order differential equation.

$$\tau \frac{dY_{(t)}}{dt} + Y_{(t)} = KX_{(t)}$$
$$\overline{Y_{(s)} = \left[\frac{K}{\tau s + 1}\right]X_{(s)}}$$

where

 $au = \frac{a_1}{a_0}$ is the *time constant* $K = \frac{b}{a_0}$ is the *steady-state gain*





Step Response

• To obtain the step response of magnitude Δx , we let $X_{(t)} = \Delta x$. The transform of the input is $X_{(s)} = \Delta x/s$. Substitute this to the equation of standard transfer function

$$Y_{(s)} = \frac{K}{\tau s + 1} \frac{\Delta x}{s} = \frac{K \Delta x}{s(\tau s + 1)}$$

- The time constant associated with this system is $\tau = 1/a$. The time constant tells how quickly the system responds.
- For example, if *a=1*, then the system responds on the order of *τ=1* second; however, if *a=100*, then the system responds on the order of *τ=0.01* seconds.
- So, systems that respond quickly have *large* values of *a*, and systems that respond slowly have *small* values of *a*.
- The 2% settling time for a first order system is $T_s = 4\tau = 4/a$.
- This represents the amounts of time required for the system to reach and stay within 2% of the final value.





Step Response

The plot below shows the step response for three different systems with a values of 0.5, 1, and 5. All systems attain a final value of 1, but note that the system with a=5, attains that value more quickly than the other two, and the system with a=0.5 attains that value more slowly than the other two. The 2% settling times for the three system are 4/5, 4, and 8 seconds respectively.







Ramp Response

- A ramp is a linear increase in the input with time starting at time zero.
- The input function is given by $X_{(t)}=at$. The Laplace transform is $X_{(s)}=a/s^2$.
- Substitute this to the equation of standard transfer function and performing a partial fraction expansion yields

$$Y_{(s)} = \frac{K}{\tau s + 1} \frac{a}{s^2} = \frac{\alpha_1}{\tau s + 1} + \frac{\alpha_2}{s} + \frac{\alpha_3}{s^2}$$

• The Heaviside expansion gives

$$Y_{(s)} = \frac{Ka\tau^2}{\tau s + 1} - \frac{Ka\tau}{s} + \frac{Ka}{s^2}$$

• Inverting yields

$$y_{(t)} = Ka\tau \left(e^{-t/\tau} - 1\right) + Kat$$

• The above expression has the interesting property that for large values of time (t>> τ) $y_{(t)} \approx Ka(t-\tau)$





Sinusoidal Response

• Processes are also subjected to periodic, or cyclic, disturbances. They can be approximated by a sinusoidal disturbance:

Hence

$$\begin{aligned}
x_{\sin(t)} &= \begin{cases} 0 & for \quad t < 0 \\ A\sin(\omega t) & for \quad t \ge 0 \end{cases} \\
& \text{where:} \quad A = \text{Amplitude,} \quad \omega = \text{angular frequency} \\
& Y_{(s)} &= \frac{KA\omega}{(\tau s + 1)(s^2 + \omega^2)} \\
& = \frac{KA\omega}{(\tau s + 1)(s^2 + \omega^2)} \left(\frac{\omega \tau^2}{\tau s + 1} - \frac{s\omega \tau}{s^2 + \omega^2} + \frac{\omega}{s^2 + \omega^2} \right) \\
& \text{Hence} \quad y_{(t)} &= \frac{KA}{2} \int_{0}^{2} \frac{\omega \tau}{2} \int_{0}^{1} \frac{\omega \tau}{\omega \tau} \left(\omega \tau e^{-t/\tau} - \omega \tau \cos \omega t + \sin \omega t \right) \\
\end{aligned}$$

$$\omega^2 \tau^2 + 1^{(0)}$$

or, by using trigonometric identities,

$$y_{(t)} = \frac{KA\omega\tau}{\omega^2\tau^2 + 1}e^{-t/\tau} + \frac{KA}{\sqrt{\omega^2\tau^2 + 1}}\sin(\omega t + \phi)$$





Response of Integrating Process Units

- Consider the model of liquid-level system with a pump attached to the outflow line.
- Assuming that the outflow rate *q* can be set at any time by the speed of the pump or by the valve in the effluent line:

$$A\frac{dh_{(t)}}{dt} = q_{i(t)} - q_{(t)}$$

• After subtracting the steady-state version of equation above,

$$A\frac{dh'_{(t)}}{dt} = q'_{i(t)} - q'_{(t)}$$

• Taking Laplace transforms

$$sAH'_{(s)} = Q'_{i(s)} - Q'_{(s)}$$

and rearranging gives

$$H'_{(s)} = \frac{1}{As} \Big[Q'_{i(s)} - Q'_{(s)} \Big]$$

• Both of the transfer functions representing integrating units, characterized by the term 1/s.





References:

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