SKF4153- PLANT DESIGN

PROCESS SYNTHESIS & CREATION

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SELECTION CRITERIA

- Thermo-physical property data
 - physical properties (T, P, conversion)
 - phase equilibria (VLE data)
 - Property prediction methods
- Environmental and safety data
 - toxicity data
 - flammability data
- Chemical Prices
 - e.g. as published in the Chemical Marketing Reporter
- Experiments
 - to check on crucial items above

Knovel website, MSDS, NIST chemical webpage, patents, etc.



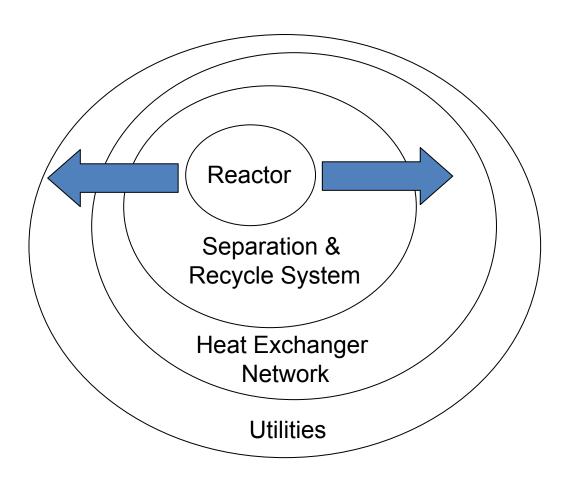
PROCESS SYNTHESIS

- © Synthesis steps (Rudd, Powers, Sirrola, 1973) -
 - Eliminate differences in molecular types (chemical reaction)
 - Distribute chemicals by matching sources and sinks (mixing & recycle)
 - Eliminate differences in composition (separation)
 - Eliminate differences in temperature, pressure and phase
 - Integrate tasks (combine tasks into unit operations)

Reference: W.D. Seider, J.D. Seider, D.R. Lewin, Product and Process Design Principles: Synthesis, Analysis and Evaluation, John Wiley and Sons, Inc., 2010.



The "Onion" Model (Smith and Linnhoff, 1995)





Synthesis Step 1: Eliminate Differences in Molecular Types

Compare advantages and disadvantages of all type of reactions possible...





RECALL

IRREVERSIBLE

REVERSIBLE

Feed1 + Feed2 → Product + Byproduct

An excess of one feed component would force another feed component to complete conversion.

Maximum conversion is limited by the equilibrium conversion

Which feed in excess?

Cost

Safety

To increase equilibrium conversion:

Adding access of one feed Remove byproduct



WHAT IF SIDE REACTION IS REVERSIBLE?

TO MAXIMIZE SELECTIVITY,
INHIBIT THE BYPRODUCT FORMATION

By using <u>excess of Feed2</u> will force Feed1 to complete conversion and inhibit the side reaction

Or, removing the product as reaction proceed will force the secondary reaction to left side and inhibit the Byproduct formation



EXERCISE

Benzene is produced from toluene,

$$C_6H_5CH_3 + H_2 \rightarrow C_6H_6 + CH_4$$

 Biphenyl, the unwanted byproduct is produced from benzene,

$$2C_6H_6 \rightarrow C_{12}H_{10} + H_2$$

| | Inlet Flow (kmol/hr) | Outlet Flow (kmol/hr) |
|---|-------------------------|--------------------------|
| H ₂ | 1858 | 1583 |
| CH ₄ | 804 | 1083 |
| C_6H_6 | 13 | 282 |
| C ₆ H ₅ CH ₃ | 372 | 93 |
| C ₁₂ H ₁₀ | 0 | 4 |

• Calculate the conversion, selectivity and yield with respect to toluene.



GROSS PROFIT EVALUATION

Monochlorodecane (MCD)
 C₁₀H₂₁Cl is produced through,

$$C_{10}H_{22} + CI_2 \rightarrow C_{10}H_{21}CI + HCI$$

 A side reaction to which unwanted byproduct dichlorodecane (DCD) is produced

$$C_{10}H_{22} + 2CI_2 \rightarrow C_{10}H_{20}CI_2 + 2HCI$$

- Calculate E.P.
- What would you suggest to increase the production yield?

| | Molecular weight | Price (\$/kg) |
|----------|---------------------|---------------|
| HCI | 36 | 0.35 |
| Chlorine | 71 | 0.21 |
| DEC | 142 | 0.27 |
| MCD | 176 | 0.45 |
| DCD | 211 | 0.00 |



Synthesis Step 2: Matching sources and sinks

How much <u>reactant</u> do we need to obtain the desired <u>production rate</u>? Can we recycle un-reacted reactant?





Synthesis Step 3: Eliminate Differences in Composition

How to <u>separate</u> desired and undesired product? Can we <u>recycle</u> to obtain <u>higher</u> production?



To eliminate differences in composition, 2 distillation towers in series are inserted. Distillation is desirable because of large volatility differences among the 3 species.

See the boiling points in table below.

| Boiling point (°C) | | | Critical | constants | | |
|---|-------|---------|----------|-----------|-----------------------------|----------------------|
| Chemical | 1 atm | 4.8 atm | 12 atm | 26 atm | $T_{c},^{\circ}\mathcal{C}$ | P _c , atm |
| HCl | -84.8 | -51.7 | -26.2 | 0 | 51.4 | 82.1 |
| C_2H_3CI | -13.8 | 33.1 | 70.5 | 110 | 159 | 56 |
| C ₂ H ₄ Cl ₂ | 83.7 | 146 | 193 | 242 | 250 | 50 |



Synthesis Step 4: Eliminate Differences in T, P and Phase

Identify all **T, P and phase change** to determine the required **utility systems**...





How do we set the T and P?

Sensible operating range to avoid severe processing difficulties

| Parameter | Range | Rationale |
|-------------|---------------------|---|
| Pressure | Between 1 to 10 bar | Most equipment can go up to 10 bar without increase in capital cost |
| Temperature | 40 to 260°C | Limited by utilities available: cooling water @ (30°C) and steam between 40 to 60 bar (260°C) |



Pressure Range

The decision to operate outside the range of 1 to 10 bar usually is a compromise between <u>performance</u> and the <u>capital and operating costs</u> of process equipment.

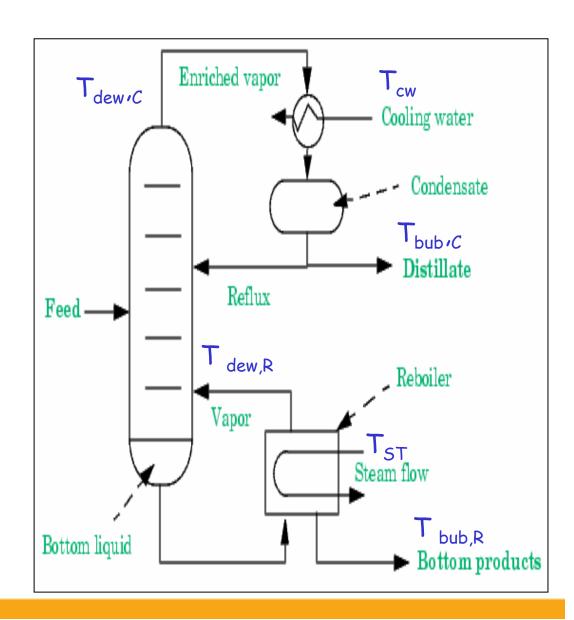
| Conditions | Justification | Penalty | |
|------------|---|---|--|
| P > 10 bar | In gas operations, increased density, lower volume, smaller equipment (for the same residence time), higher quality heating media (steam) | More costly, thicker- walled equipment needed | |
| P < 1 bar | Prevent degradation of <u>heat-sensitive</u> <u>materials</u> | Larger equipment. Need special equipment construction for vacuum operations | |



Column Temperature

Primarily dictated by cooling water temp., Tcw:

$$\begin{aligned} &T_{CW} \leq T_{bub,C} \leq T_{dew,C} \leq T_{bub,R} \\ &\leq T_{dew,R} \leq T_{ST} \end{aligned}$$





Synthesis Step 5: Integrate Tasks

Complete the **unit operations**...





Process Equipment Identification

| Process Equipment | General Format XX-YZZ A/B | |
|--------------------------|--|--|
| | XX are the identification letters for the equipment classification | |
| | C - Compressor or Turbine | |
| | E - Heat Exchanger | |
| | H - Fired Heater | |
| | P - Pump | |
| | R - Reactor | |
| | T - Tower | |
| | TK - Storage Tank | |
| | V - Vessel | |
| | Y designates an area within the plant | |
| | ZZ is the number designation for each item in an equipment class | |
| | A/B identifies parallel units or backup units not shown on a PFD | |
| Supplemental Information | Additional description of equipment given on top of PFD | |

Consider P-101A/B:

P-101A/B identifies the equipment as a **Pump**

P-101A/B indicates that the pump is located in **Area 100** of the plant

P-101A/B indicates that this specific pump is <u>number 01</u> in Area 100

P-101A/B indicates that a **back-up pump** is installed. Thus, there are two identical pumps,

P-101A and P-101B. One pump will be operating while the other is idle.



EXERCISE

Monochlorodecane (MCD) C₁₀H₂₁Cl is produced through,

$$C_{10}H_{22} + CI_2 \rightarrow C_{10}H_{21}CI + HCI$$

 A side reaction to which unwanted byproduct dichlorodecane (DCD) is produced

$$C_{10}H_{22} + 2CI_2 \rightarrow C_{10}H_{20}CI_2 + 2HCI$$

 Develop a process flowsheet according the 5 synthesis steps.

| B.P @ 1 atm | Molecular weight | Boiling Pt. (K) |
|-------------|---------------------|--------------------|
| HCI | 36 | 188 |
| Chlorine | 71 | 239 |
| DEC | 142 | 447 |
| MCD | 176 | 488 |
| DCD | 211 | 495 |

Assume:

- ❖ Incomplete conversion of both feed.
- Reaction at 152 K, 2 atm.
- Feed to the first separation is at 200K, 10 atm.



SUMMARY

Key information (materials and products)

- Thermo-physical property data
- Environmental and safety data
- Chemical Prices
- Batch or continuous operations
- Unit operations involved

Key steps in designing a process plant

- Chemical reaction
- Mixing & recycle
- > Separation processes
- Eliminate differences in temperature, pressure and phase
- Integrate tasks (combine tasks into unit operations)



References

- J.M. Coulson, J.F. Richardson, R.K. Sinnot, Chemical Engineering Vol. 6, Pergamon Press, 1985.
- J.M. Douglas, Conceptual Design of Chemical Processes, McGraw Hill, 1998.
- L.T. Biegler, I.E. Grossman, A.W. Westerberg, Systematic Methods of Chemical Process Design, Prentice Hall, 1997.
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